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Automated Material Testing

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Abstract

In order to exponentially increase the capabilities of the material testing team at Volvo Cars, a deep exploration of automated testing solution was conducted. Firstly, a complete 3-point bending automated cell was developed, able to perform tests according to VDA 238-100 standard and collect results without human assistance. Secondly, possible expansions will be considered, with particular attention on the adaptation necessary to perform tensile tests. Several key challenges are explained, and all the technical solution presented in order to optimize testing efficiency. The knowledge gathered is the starting point for allocating investments into advanced automated testing systems for industrial applications.

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Abbreviations and Acronyms

PLC	Programmable Logic Controller
DI	Digital Input
DO	Digital Output
AI	Analog Input
AO	Analog Output
TCP	Tool Center Point
FBD	Function Block Diagram
DIC	Digital Image Correlation
CT Scan	Computed Tomography Scanning

Chapter 1

Introduction

Manually testing the properties of raw materials is a time-consuming and repetitive process. The operator is required to measure each sample one by one, set up the testing equipment properly and evaluate the results. This process is not feasible for batches of hundreds of samples. Manual labour is also affected by human error and data will be subject to slight variations. In such situations the presence of an automatic station makes data collection more precise and in a fraction of the time. The aim of this paper is to guide you through the necessary steps to set up a functioning automatic 3-point bending test cell and discuss the possibilities of automation of other test types, such as tensile.

1.1 Contextualization of the thesis work at Volvo Cars

At the Volvo Cars facility, in Göteborg Sweden, a small material testing team is responsible for handling all the requests from the other departments. Understanding material properties is a crucial step in the research process to develop new material and are required in many simulations for accurate results.

This project is the starting point to understand the capabilities of automated setups, evaluate the challenges along the way and consider whether allocate investments in the future. The vision is to have an advanced laboratory able to test several different sample types and collect data in the most efficient way.

1.2 Aim of the project and evaluation parameters

The project aims at understanding and evaluating the challenges in having an autonomous laboratory. Every step automatized allows the operator to concentrate on higher-value tasks, such as attending a meeting. The steps to be automated are the sample measurement, the testing phase and data collection. Some steps will still require manual labour. These are obtaining samples, labelling them with QR code stickers and analysing the obtained data.

The project is divided in two parts. Firstly, a complete bending test cell is to be developed. 3 point bending was chosen for the easier manoeuvrability of the samples, especially after the testing phase. In doing so the goal is to understand what the main challenges are and the component needed. This system will then be evaluated by obtaining real data and comparing it with results obtained manually.

Secondly, an exploration of the required changes for the tensile test can take place. The goal is to adapt the system to handle both types of test. This part is evaluated by the variety of testing types that can take place.

1.3 Analysis of already existing systems

Materials can be described using a variety of testing procedures, depending on the sort of information needed and the intended use. Destructive testing techniques are commonly used to determine mechanical parameters such as yield strength and Young's modulus [2],[3].

Automated testing becomes particularly useful when dealing with a large number of samples or when great precision and reproducibility are required. Given the specialized nature of such systems, only a limited number are now accessible and thoroughly documented in the literature [4, 5].

Several stations to perform automated material testing have already been developed [6],[7],[8]. This setups thought, don't fully take advantage of the speed capabilities of the cell, designed to be used only for a limited number of samples. This type is more directed towards standardization, rather than throughput and aim at replacing a knowledgeable operator. Larger systems exist for tensile testing [9, 10, 11, 12]. They are custom built for the specific laboratory and its requirement. Examples range from preserving the fracture surface, to measuring all the dimensions, or even execute multiple tests on the same sample.

Chapter 2

Automated bending system

The following chapter explains the development of the 3 point bending test cell and considerations to be made in order to set up a functioning test cell. The overview ranges from choosing the appropriate components to use, to integrating them to work seamlessly together. Particular attention will be dedicated to ensuring test precision, and validating the accuracy of test results obtained. Finally, potential challenges in system integration, troubleshooting, and optimization of throughput will be addressed, setting the stage for a successful implementation of the bending test cell [13].

2.1 System requirements

The bending test cell had to satisfy the following requirements. Firstly, tracking each sample is needed, avoiding manually written labels and allowing the reconstruction of each sample's history from cutting from the base material to the test data. Preserving the sample after the test is also beneficial, in case the results are outside expectation, visual inspection of the fractured surface can take place. The required precision during execution is moderate. What the robot provides is inside the acceptable limit and can be further increased utilizing all the hardware capabilities. Therefore, the aim will be on productivity. The data obtained from the 3-point bending test is mainly the bending angle. Maximum force applied and estimation of Young's modulus are an added benefit.

2.2 Test setup

The VDA 238-100 standard for three point bending of sheet materials is widely adopted to assess local formability [14],[15]. The standard specifies

geometric constraints, including the size and shape of the fixture, as well as the punch dimensions. A diagram illustrating the geometry is provided in Figure 2.1. In addition, the standard outlines test execution parameters to use, such as preload, all the stopping conditions and speed settings to be utilized at each step of the process.

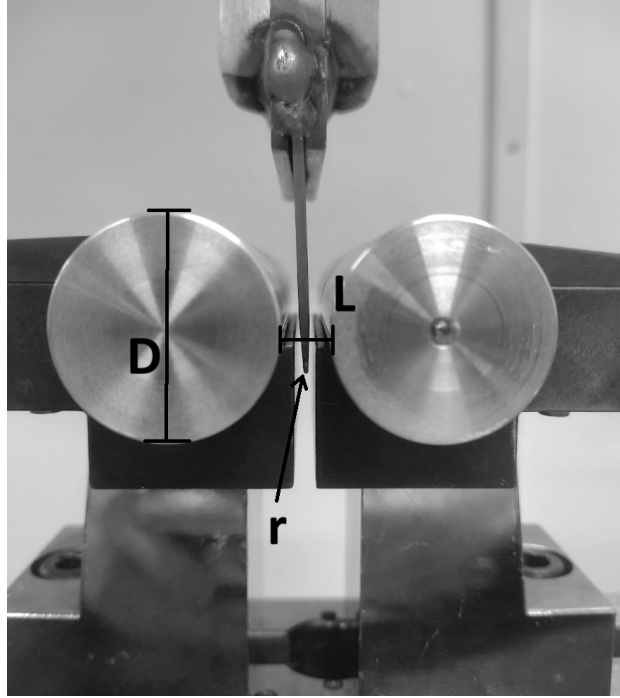


Figure 2.1: Geometry used according to VDA 238-100

The 3 point bending test is performed with $60\text{ mm} \times 60\text{ mm}$ square-shaped samples. Thickness is a crucial parameter in bending and will therefore be measured more accurately for each sample individually during the testing cycle. The distance between the rollers L is a function of the sample thickness t_m . The available fixture used does not allow robotized changes and will therefore have to be fixed in position. Since all samples have a nominal thickness of approximately 3 mm the roller distance is set to 6.09 mm. This decision has also been taken to not introduce variations with the reference data in the results (see Section 2.13). The rest of the parameters are according to the standard and precise values are shown in the Table 2.1 below.

Symbol	Description	Value [mm]
r	Punch radius	0.4 ± 0.02
D	Roller diameter	30 ± 0.01
L	Roller distance	6.09 ± 0.1
b	Sample width	60 ± 2
l	Sample length	60 ± 2
t_m	Sample thickness	Measured for each sample

Table 2.1: Test parameters

2.3 Layout

For organization purposes, a sketch of the layout is necessary. The whole system will have to be placed inside the robot arm reach of 950 mm. The layout, shown in Figure 2.2, includes several key areas, each fulfilling a distinct role within the automated cycle. A pick up station is the location where samples are stored and where the robot grabs one sample after another. The QR code station is where sample recognitions takes place through a QR code sticker. Measurement station is dedicated to evaluating the sample's thickness. At the testing station the sample is positioned and test execution can take place. Finally the disposal station is where the sample is deposited after the testing has occurred.

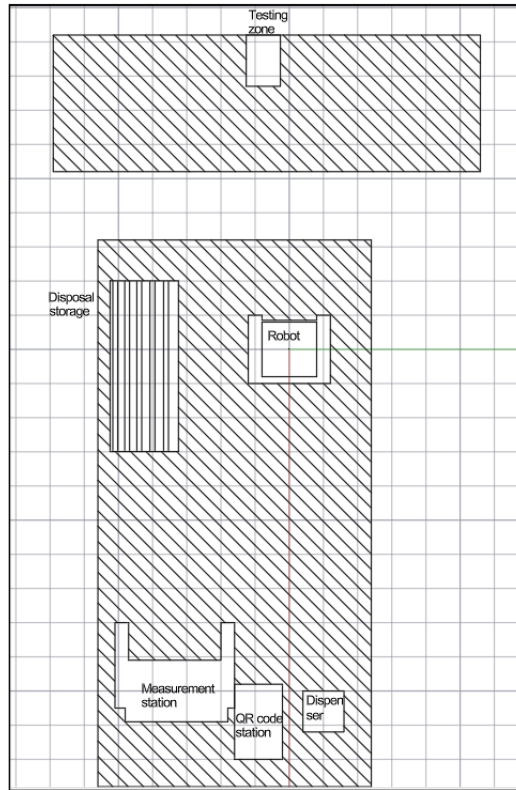


Figure 2.2: Layout plan showing all stations and their relative position.

The layout is in scale, to have a clear idea of the available space for manoeuvrability and the overall appearance of the cell.

2.3.1 Coordinate systems

Several coordinate systems exist and can be either fixed or moving. The main one is the world coordinate. It is fixed and placed in the centre of the robot base. It's the one being used for all object position in the x-y plane represented in Figure 2.2. This way it is easy to access the coordinates of a certain point of station relative to the robot. This same coordinate system is being used for the virtual Robotstudio setup.

The TCP coordinate system is instead a moving system that stays consistent to the tool centre point and is used for tool position when reaching targets. When defining a new tool, a new set of TCP coordinates is created in the specified location. The Work object coordinate system also exists. It is used in case of operations done on and around the work object, in order to stay consistent to it, while ignoring everything else. This has not been necessary to implement.

2.4 Robot setup

The robotic arm plays an important role in moving the sample between the station and ensuring smooth operation can take place. It is managed by the robot controller, which executes the program, sends and receives signals, and deals with errors. At the end of the arm a tool, controlled by the robot, is used as interface with any work-objects, in this case being the test sample itself. This final component of the robot has to be custom made for the application and then defined in the program. It is discussed in Section 2.4.4.

2.4.1 Robot specification

The robot used is an ABB cobot (collaborative robot) CRB 15000 [16]. It has an arm reach of 0.95 m and 6 degrees of freedom. The absolute position accuracy of 0.1 mm ensures the required precision is reached. The maximum payload of 5 kg is not a limiting factor, nor is the maximum speed of 2.2 m/s of the TCP (Tool Center Point) [17]. A visual representation of the robot arm is shown in Figure 2.3.

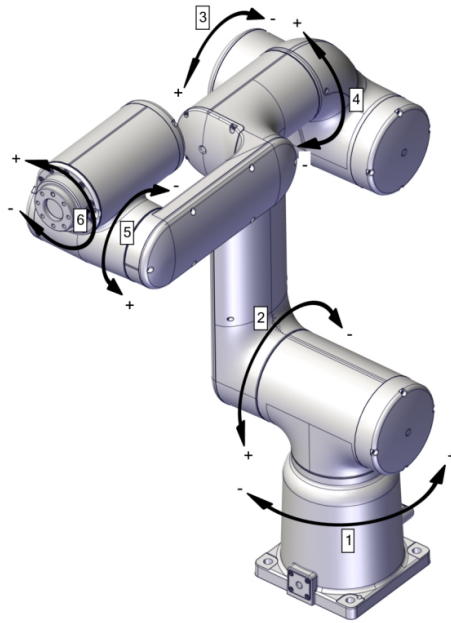


Figure 2.3: Robot schematic [1]

Being a cobot, it has force and torque sensors to stop movement in case of contact with a human or an unexpected object. This feature will also be

used for force dependent operations.

The available signals are 16 DO, 16 DI, but no analog input or output is available directly in the robot controller. The robot includes a FlexPendant [18] as interface directly with the robot controller. It is used to visualize uploaded programs, monitor execution and perform jogging operations.

2.4.2 Safety configuration

The robot requires safety configuration in order to operate properly. This settings are implemented in the form of safety zones which enforce either speed or force limitations and need to be tuned correctly in order to avoid encountering any risks.

Beyond zone configuration, comprehensive safety involves performing a risk assessment in compliance with industrial safety standards such as ISO 10218 [19],[20] for industrial robots and ISO/TS 15066 [21],[22],[23] for collaborative applications [24].

2.4.3 Programming

The robot program is written in RAPID [25], a high level language developed by ABB specifically for robots. The compatible computer program is Robotstudio, developed by ABB as well, which allows to freely modify the code, model the station in a 3D environment and simulate the current setup. Points of interest have to be defined at the beginning alongside all tool data and variables [26, 27]. Obtaining robot target can be done by jogging or the lead through functionality of the cobot, as well as defined manually. It's important that all target not only clarify the position in space, but also the orientation of the tool in that position.

Figure 2.4 shows the 3D modelled station inside RobotStudio.

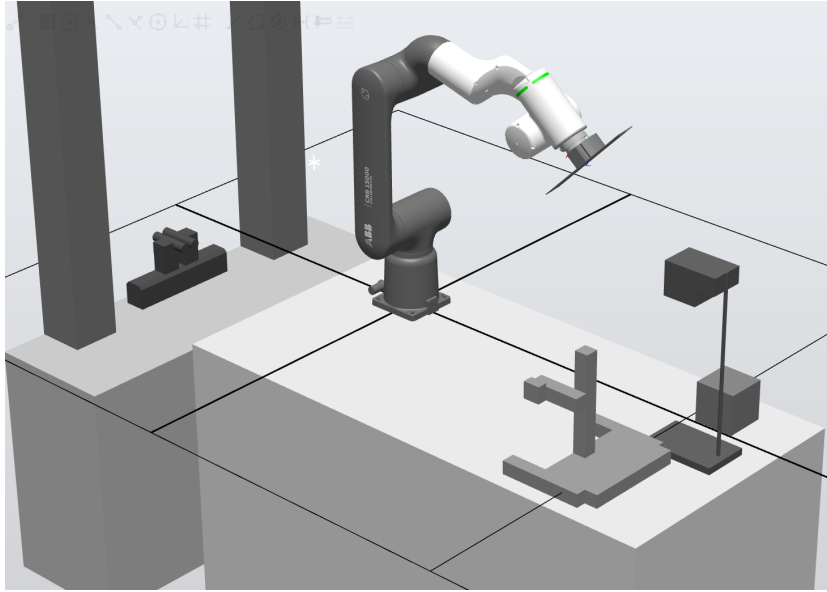


Figure 2.4: Modelled station implemented in RobotStudio.

At the beginning of the programming process, key points of interest, as well as all necessary tool data and variables, must be defined. The robot targets can be specified either through jogging, using the “lead-through” functionality of the robot, or manually. It is crucial that each target not only defines the robot’s position in space but also the orientation of the tool at that position.

The program is also responsible for overseeing and altering all signals states in the controller and determines the pace of the whole cell by monitoring the measurement process and test execution.

To facilitate debugging and improve code understanding, the use of functions is essential. By invoking functions only when necessary, it is possible to reuse, adapt, and organize code sections more effectively. The program is executed cyclically an indefinite number of times unless otherwise specified. See Appendix C.3 for the full program.

2.4.4 Tool

The tool, or end effector, is an extremely important component in the robot setup. It is fixed at the end of the robot arm and is the interface between the work object, test samples in this case. It is composed of two components, the tool exchanger and tool head.

The tool exchanger is a small cylindrical component which itself is composed of two parts. The tool attachment is fixed and attaches directly to the

end of the robot arm. It receives all electric signals from the controller and air tubes. The tool exchanger instead has the role of passing all signals and air connections to the tool head, while also being detachable. The specific part used was provided by Robot system product, Coboshift tool attachment MTA18 and Coboshift tool changer MTC18, which allows a total of 6 electrical connections alongside 4 air ducts [28]. The tool exchanger used is manual, but automatic solutions exists as well.

The tool head was designed in a 3D cad software to fit onto the tool exchanger with 4 screws. The developed solution is composed of two sides (see Figure 2.5). The first houses two suction cups used to handle the samples before they are tested. The second manages the bent samples after the test has been executed with a vacuum gripper. The suction cups, vacuum gripper, and vacuum controller were all provided by Piab. Modelling the tool head is essential in case of 3D printing requirements. It is beneficial in all other cases to get accurate dimensions, import it in Robotstudio and adapt the safety configuration correctly. Figure 2.5 below shows both the 3D CAD model and the corresponding physical object.

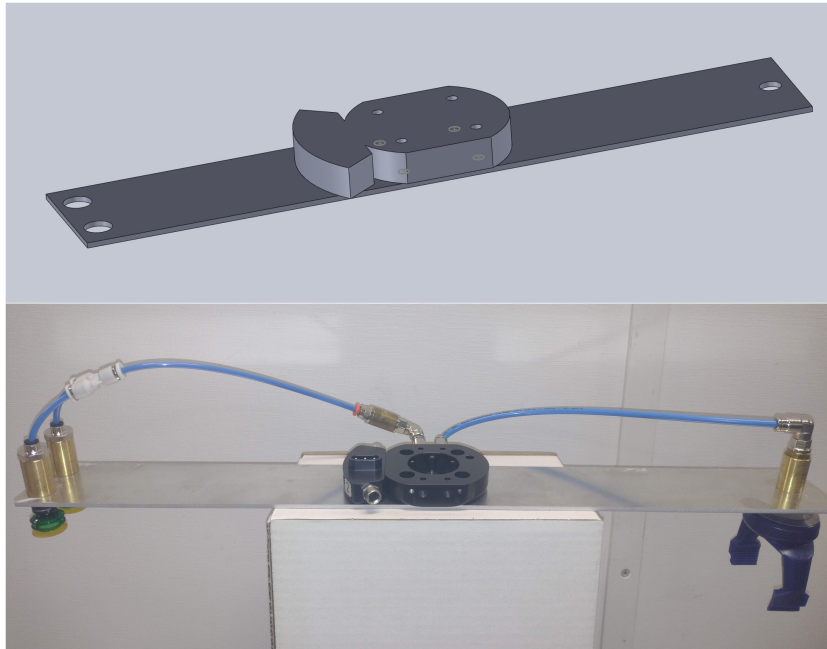


Figure 2.5: Virtual model (above) and physical tool (below).

2.5 Pick up station

For correct usage of the testing cell, the operator is required to cut, label and position the samples to be tested in the storage location before turning the system on. As storage, several solutions can be utilized, but the simplest is the most effective. Samples need to be stacked on top of each other in a specific location recognized by the robot. All successive operation are carried out without further input.

The x and y position of the sample stack needs to be defined, as the robot relies on a searching routine to detect the correct vertical distance. Once the appropriate proximity is reached, the sample is lifted off by the negative pressure in the suction cups, even before coming in full contact, and is securely attached to the tool. Although this approach results in some loss of positional precision, it is acceptable at this stage, as high accuracy is not critical during the initial pickup. However, adjustments must be made to eliminate this uncertainty before placing the sample onto the test fixture, where precise positioning becomes essential for reliable test execution.

In case the sample stack is too high, a multiple stack approach is possible. Using the same principle stack number 2, 3 etc are processed correctly. When starting the program for the first time it's required to input the number of samples in each stack, so that counting the number of cycles executed, it's possible to process every sample.

2.6 QR-code station

The QR code station is composed of a camera and a space for the robot to show the sample to the field of view. The camera is then connected to the computer running a Python script continuously. The purpose of the code is to analyse frame by frame the camera feed, recognize any QR codes present and decode it through the OpenCV library [29]. The QR code contains informations regarding the previous operations each sample has been through. For simplicity purposes it contains the sample number, but can be expanded if required. Each time a new QR code is detected, the code creates a new excel sheet containing introductory column labels and the sample number in the first row. Each cell will then be filled with correct information, already converted into the appropriate measurement unit.

The most critical parameter to adjust, to ensure smooth operation, is the focus point of the camera, as QR-codes not in focus might not be recognised by the camera. Although this is a rare occurrence, placing the camera at 15 to 20 cm from the ground surface can help minimize errors.

2.7 Measurement station

The measurement station, shown in Figure 2.6, is where thickness is evaluated. That is a important parameter in the bending test and needs to be precisely determined. As for the other dimensions, they are not crucial for the bending test, and will not be measured for each sample individually, but an estimation will be given. The measurement process involves calculating the distance difference between when the sample is present and when is not. This way thickness values are extrapolated. To do so, a laser is pointed downwards and a detector is able to evaluate distance based on triangulation angle. The device being used is a CP35MHT80 [30] high performance sensor, capable of 0.05 mm resolution. The output is in the form of a voltage analog signal from 0 to 10 V. Calibration of this device was performed with objects of known thickness, to then construct a calibration line (see Appendix B.1) [31, 32].

This station is positioned at an angle. This is because each sample is dropped and guided by gravity to a specific corner of the station. This way it's possible to eliminate any variation of position in the pick up sequence and increase placement precision when executing the test. Grabbing the sample after this stage is a delicate process as precision is required. For this reason force control was used. This robot functionality allows to preset a path and a force goal in the z direction. When the load is reached the program skips to the following steps. The force limit is set to 5N. This way any imprecision in the lifting sequence is minimized.

The method chosen is not optimal in terms of accuracy and cannot take into account curved samples. Solving this issue involves more advanced equipment to take measurements from both sides [33]. This laser measurement solution was selected for convenience and the possibility to be combined with the alignment.

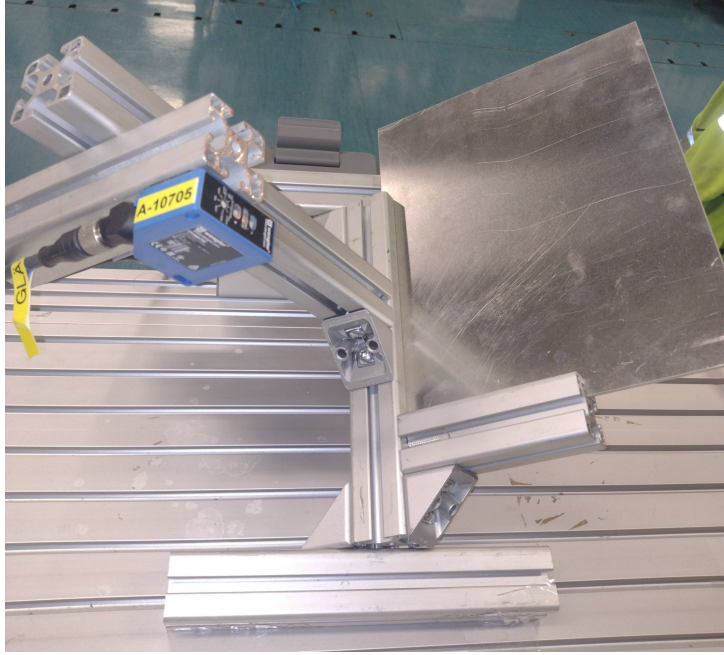


Figure 2.6: Measuring station

2.8 Testing station

The test procedure involves several steps and safety checks in order to proceed. Firstly the sample is placed onto the fixture with high precision. Position confirmation is verified with another laser (similar to the one used during measurement calculation) pointed upwards, ensuring the presence of a test sample. The machine used is the MST Alliance RF/100 [34] (see Appendix A.3) for tension and compression with a Load cell up to 100 kN.

The test procedure starts with a preload phase at lowering the crosshead at 10 mm/min, followed by a main loading phase at 30 mm/min. To accurately determine the bending angle, it is essential to isolate the plastic deformation by removing the influence of elastic recovery. This is achieved by introducing an additional unloading phase following the previously described loading sequence, by moving the crosshead upwards at a rate of 10 mm/min until the applied load approaches 0 N. At this point, the system performs a 5 second hold to allow for stabilization and to record the crosshead displacement, before returning to its initial position. This additional step ensures that the displacement value used for calculating the bending angle reflects only the plastic deformation, excluding any contribution from the elastic one.

Several mathematical models exist to determine the bending angle α_c

in degrees from the crosshead displacement. The standard VDA 238-100 provides the set of equations to use:

$$\alpha_c = 2 \left\{ \cos^{-1} \left[\frac{W \cdot p - c \cdot (S - c)}{p^2 + (S - c)^2} \right] \cdot \left(\frac{180^\circ}{\pi} \right) \right\}, \quad (2.1)$$

where:

$$W = \sqrt{p^2 + (S - c)^2 - c^2}, \quad (2.2)$$

and:

$$c = \frac{D}{2} + t_m + r. \quad (2.3)$$

Here, S is the crosshead displacement after preload, while the other parameters are described in Table 2.1 (see Appendix C.2, Lines 124-131 for the implementation into the program). Although mathematical models are based on analytical formulas and experimental errors are unavoidable, independent assessments and literature reviews found the angle prediction to be reasonably accurate, typically underestimating by up to 5° [35, 15, 36].

The testing sequence is triggered by a single digital input, while data acquisition is handled through two analog outputs, one for crosshead position and one for applied load. Both outputs are calibrated within the 0–10 V range and are interpreted by the PLC. During the test, the robot tool rotates into position, and once the crosshead returns to its initial state, the vacuum gripper is activated to safely remove the tested sample from the fixture.

2.9 Disposal station

The purpose of the disposal storage, shown in Figure 2.7, is to house all the tested samples in order, while not damaging the surfaces. Following the design philosophy of making things simple, strips of plastic were glued to a base so that samples can be dropped from the top and remain in an upright position. One after the other each sample is placed in a grid separated from the others. Based on the completed cycle number each sample is positioned in the correct location. Completed this step the system resets itself and a new cycle can start.

The number of storage slots in the disposal station is also the limiting factor for the maximum number of samples that can be processed without supervision. Increasing the capacity requires the physical expansion and the corresponding adaptation in the code.

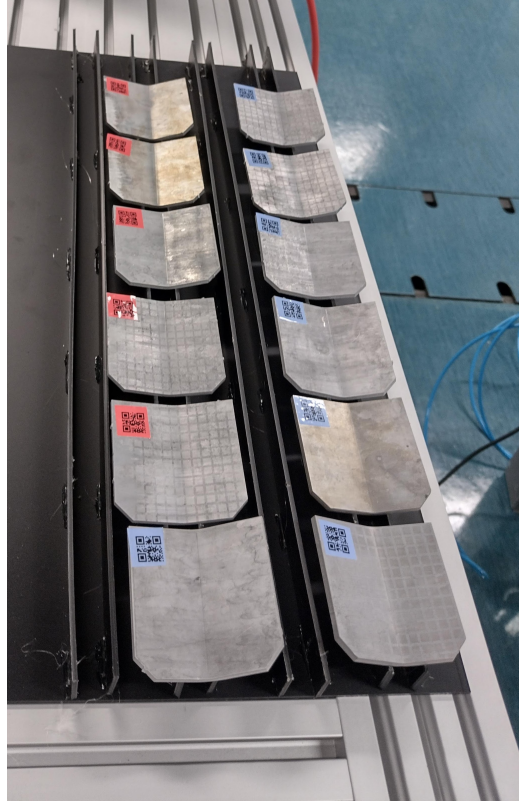


Figure 2.7: Disposal station showing 12 processed samples.

2.10 Signal handling

In order to communicate between the robot controller, the PLC and the other components in the system, several signals were used. Digital inputs and outputs are 24 V switches, either on or off. Analog signals instead can carry any voltage between 0 and 10 V. In the Figure 2.8 below all signals utilized are shown, specifying the entry port when needed. The main components are the robot controller, PLC and PC, exchanging signals with the end effector, MTS testing machine, laser sensors and QR-code camera, while in Table 2.2 the signal use is explained.

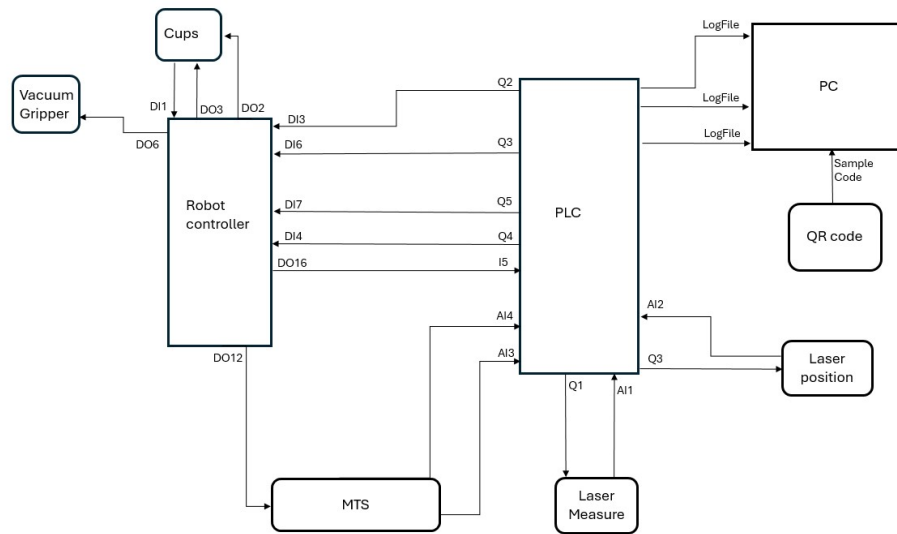


Figure 2.8: Signal map

Name	Type	From	To
Activate vacuum	Digital	Robot controller DO2	Suction cups
Activate blow-off	Digital	Robot controller DO3	Suction cups
Is vacuum on	Digital	Robot controller DI1	Suction cups
Activate gripper	Digital	Robot controller DO6	Vacuum gripper
Measurement is OK	Digital	PLC Q2	Robot controller DI3
Test finished	Digital	PLC Q5	Robot controller DI7
Sample position OK	Digital	PLC Q4	Robot controller DI4
Test type	Digital	Robot controller DO16	PLC I5
Execute test	Digital	Robot controller DO12	MTS machine
Crosshead position	Analog	MTS machine	PLC AI3
Load applied	Analog	MTS machine	PLC AI4
Execute measurement	Digital	PLC Q1	Laser measure
Thickness	Analog	Laser measure	PLC AI1
Do position check	Digital	PLC Q3	Laser position
Position	Analog	Laser position	PLC AI2
Thickness	Ethernet	PLC Ethernet LAN2	PC LogFile
Crosshead position	Ethernet	PLC Ethernet LAN2	PC LogFile
Load applied	Ethernet	PLC Ethernet LAN2	PC LogFile
QR-code data	USB	Camera	PC USB1

Table 2.2: Signal connections

2.10.1 PLC

The requirement of a PLC arises since the robot controller doesn't have any analog signals port. Also real time communication with the computer becomes a possibility, allowing to send data and analyse it with Python. The PLC used was LOGO! 8.3 [37]. The program is written in Function Blocks Diagram (FBD) and then uploaded onto the memory (see Appendix C.1).

The PLC used has some limitations that need to be solved if precise operations are required. Firstly, by default every analog signal is translated into a value from 0 to 1000. This is not enough granularity is some application and is a problem for obtaining precise measurement. Secondly, the communication is only one-way, from PLC to PC by reading all the memory cells every 0.5 seconds. Communication in the other way is not available and a more advanced system is required.

2.11 Data handling

During operation a python script is continuously running in the background (see Appendix C.2). It's role is to select and elaborate data sent from both the PLC and the camera, while also generating the excel sheet with the data gathered. Upon the detection of a new QR code, a new line is created in excel containing the sample code. During operation a CSV file named LogFile is created with a new line every 0.5 seconds containing all the current PLC memory cell values. This includes both digital state (high or low) and analog value. Performing calculation with this values allows to upload the correct reading for thickness, bending angle, max force and slope of the curve in the elastic region.

2.12 Error and safety

In order to ensure that the whole system runs smoothly, not only several safety checks are necessary, but also, in case of encountered errors, the system should reset itself to not stop operation completely.

The most errors encountered were in the robot utilization due to movement or speed restrictions. Safety related errors, for example contact with a human, will stop operation immediately and the system will not restart. Any other mistakes in the robot code are handled by the error handler function (see Appendix C.3, Line 91). This function has the role of trying to resume operation and reset the system for a new cycle to start. The error handler is either called automatically if an error occurred, or manually by raising a

custom error when required.

To make sure the sample being processed is suitable, after the thickness measurement the signal DI3 (measurement OK, 2.2) is activated only if the received values is in between predefined limits. This ensures no sample is tested if outside the 1 to 5 mm range.

A position check is executed before performing the test. With the use of a laser the signal DI4 (position is OK, 2.2) is ON only if a sample is present. During the execution of the test limits to the force applied make sure not damage is done and stop operation in case the load limit of 10000 N is reached.

Since the python code is running continuously, errors are displayed on the terminal, but don't stop execution. The most common type of errors are faced during startup of the camera, opening of files and executing calculations.

2.13 Results

The developed cell was evaluated by comparing two datasets. The first one was obtained utilizing the automatic system, while the second one by manually testing samples originating from the same component in cast aluminium. By processing the same material, the objective is to isolate and evaluate only test execution. The system performed as expected and collected thickness measurement, bending angle and peak force for all 12 samples. In Table 2.3 the values of bending angle and peak force are displayed in order for comparison between the two test methodologies.

Method	Mean Bending Angle [°]	Std Dev Bending Angle [°]	Mean Max Force [N]	Std Dev Max Force [N]
Automatic	23.3	3.9	5577	686
Manual	24.9	3.7	5491	649

Table 2.3: Comparison of mean and standard deviation

The automatic system being tested showed reasonable accuracy of results, as the variation between the results is minimal. The standard deviation can be interpreted as a measurement of the variance in test execution together with variations due to the material itself [38, 39]. For this reason by testing the same material the goal was to eliminate the material variance and establish the precision in test execution, theoretically better when the automatic

setup is used. Although similar, the standard deviation for both bending angle and max force is higher in the autonomous system compared to manual execution. Factors other than repeatability of testing might have played a role. For example, 24 samples were tested manually, compared to only 12 automatically. Also, lower quality of the original material was used in the automatic test. These variables might have driven higher standard deviation, even with similar or better precision during testing.

Cycle time was also calculated while operating the automated bending test cell. Slight variation occurred in the pick up, testing and disposal procedure, but the average cycle time was found to be 176 seconds.

The thickness of the 12 samples automatically processed, was evaluated both manually and by the system itself. Here noticeable discrepancies were observed. The mean difference between the two measurement was 0.19 mm. Considering the nominal thickness of 3 mm a variation of 6% is unacceptable, especially as it plays an important role in interpreting results and calculating flexural strength. This error is entirely caused by the LOGO! PLC converting incoming analog signals in a range of numbers from 0 to 1000. This is not an issue in most application, but in this use case greater granularity is required to enhance precision. The same problem also presents itself when interpreting the other incoming analog signals, such as force and crosshead data. The workaround is to calibrate the output in the machine itself around the interest points, in order to have greater granularity when is needed (see Appendix B.2). This is not a configurable option in the laser.

2.13.1 Imperfections

Aluminium components obtained from casting are subject to several types of internal defects, greatly affecting the mechanical properties. They are grouped into several categories depending on the cause, such as shrinkage, gas-related, filling-related, undesired phases, thermal contraction and metal-die interaction [40]. The main result is the generation of internal porosity, mainly originated by shrinkage behaviour of the material and gas entrapment. They acting as a stress concentrator, lowering the component performance under tension loads.

Detecting these internal defects in cast metal components typically requires expensive equipment and time-consuming procedure. The most common methods are ultrasonic testing [41], X-ray Radiography [42], and Computed Tomography (CT) Scanning [42]. Therefore, identifying a correlation between porosity and another measurable quantity could help determine which samples warrant further analysis.

Dispersed microporosity is known to strongly influence mechanical prop-

erties, especially by drastically reducing ductility and strength of the material [43, 44, 45] While the literature is rich for tensile test, little is known about the effect of porosity on bending test results.

In this study, the only data obtained from the automated system were bending test results, including bending angle and maximum force. To investigate potential correlations with porosity, the 12 automatically processed samples were CT scanned and are shown in Figure 2.9. The results plotted in Figure 2.10, were analysed to assess any relationship between porosity and the mechanical test data.

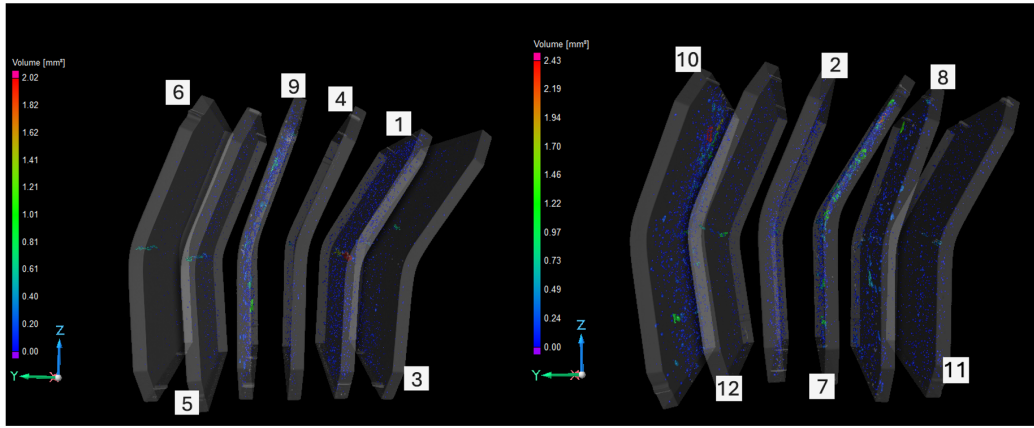


Figure 2.9: CT scan of the samples from 1 to 12.

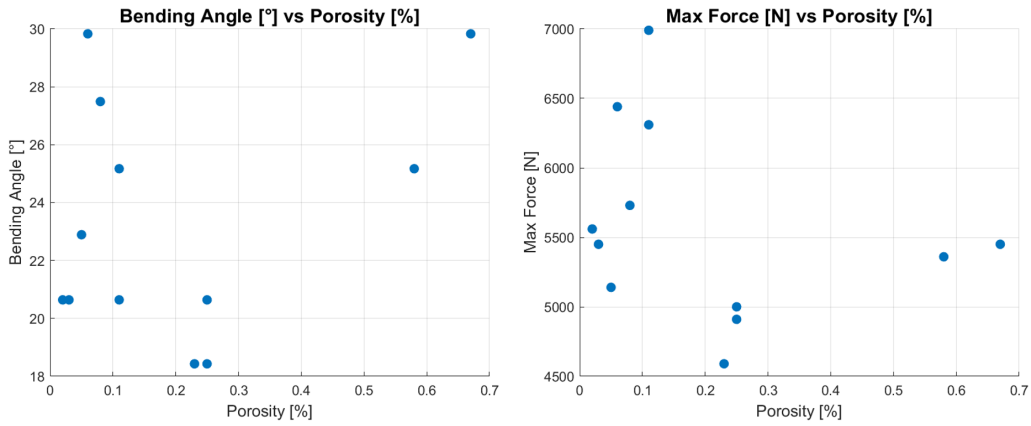


Figure 2.10: Data for bending angle (left) and max force (right).

The correlation coefficient (r value) for bending angle and porosity is 0.3, while for max force and porosity is -0.29. This indicates a vague trend for

both cases, but not strong enough to make any reliable predictions. In order to determine any relationship, further evaluation is required with more data points [46, 47, 48].

Chapter 3

Automated tensile system

The system can be expanded in several different ways. One option is to adapt the system to process a wider variety of sample shapes and allow application in a more diverse use cases. Another option is to extend the number of steps performed by the robot while reducing the ones executed by the operator, for example automatic sample labelling. The third option is to expand the capabilities and perform different test types by modifying the system to accommodate different procedures. In any case, the current system should not be compromised and possibly be used at any moment.

Even if the main focus of the project was dedicated to the development of the automated three point bending test cell, other test types were also examined for automation. Since the tensile test provides some of the most useful properties, such as Young's modulus and yield strength [49], it has the highest priority to be automated as well.

Due to the limited time-frame of the project, this second section is less developed compared to the bending test cell. Nevertheless, the progress achieved and the insights gained are presented in the following discussion.

3.1 Requirements

Several key requirement from the bending test are still valid for the tensile test, for example, preserving samples to inspect the fractured surface and tracking with QR-code is not to be neglected. Differences arise when considering that the strain field during test execution is monitored by painting dots on the surface and interpreting data with a DIC software. For accurate results, the surface must exhibit suitable properties such as elasticity and adhesion [50]. For this reason, the surface is extremely delicate and needs to be handled accordingly [51, 52].

3.2 Test Setup

The machine is composed of two grippers, able to regulate the pressure at which to close when the specimen is inserted and the camera for strain field measurement with DIC. There is a specific sequence to follow to ensure proper test results.

First, the sample is inserted into the lower gripper and secured in place. Secondly the testing procedure is started and an approach path is responsible of lowering the upper gripper in place. Thirdly, while the upper gripper is being closed, the crosshead position has to be adjusted to not induce any compression stresses prior to test execution. Once all the conditions are met, it is possible to drive the machine up to the breaking point.

To finish the procedure, the crosshead arrives to a preset position for correct handling with the robot.

3.3 Robot Setup

The robot used is the same as in the previous section 2.4.1. Being mounted on a movable platform, it can be transported in different locations for different test types. This way the bending test cell remains available to use by moving the platform back in place. To execute different test the whole robot code had to change. Firstly, when starting the system for the first time, the user is required to choose between the different test types available (currently bending and tensile). Following this decision the correct section of the code is selected.

The preferred test type is then communicated to the Python script via the PLC, making sure that the appropriate part of the code is executed.

3.3.1 Tool head

Accommodating the new sample shape (see Appendix A.2) requires an appropriate end effector. This component was designed to grab tensile test samples without damaging the painted surface. The padded jaws from Piab (specifically the GRZ 10-10 NPC-P [53]) was mounted at the tip of the end effector, and a distance laser sensor was integrated to monitor the separation between the gripper jaws in real time. The final version of the end effector used in this setup is shown in Figure 3.1.



Figure 3.1: Tool used to handle tensile test samples.

3.4 Robot-Machine communication

The robot has to be able to control the machine grippers during the opening and closing sequence, and also start the test execution at the appropriate moment. This can be controlled by turning on the correct digital signal for a specific amount of time. In my case 3 seconds is enough to securely grip samples. The I/O interface is used to communicate with the machine to start and then monitor test execution.

3.5 Disposal

The final step of the cycle is the removal of both sides of the broken sample from the machine grippers. This step can prove to be particularly challenging, for the unpredictability of the breaking point along the sample length. To solve this problem, the distance laser sensor is utilized. The robot moves in a trajectory towards the sample lower part until the correct distance is achieved. After the robot secures the part, the lower machine gripper can

be opened and the first part disposed in a predefined location. The same procedure can be adapted for the upper section.

Chapter 4

Discussion

The use of a cobot in mechanical testing proved to be valuable, by increasing consistency and reliability of test execution. Although promising, a long development phase is still required to achieve the final goal of a automatized laboratory. The project proved the possibility and potential of robotized testing, as well as highlighting some of the challenges. A separate discussion is provided for the bending and tensile test setups.

4.1 Bending test system

The implementation of a robotic station for automatic 3-point bending was successful and can now be used in every day tasks. The real advantage is in terms of time saved and throughput. The operator spends between 10 to 15 minutes on average to measure a sample, set up the machine configuration, execute the test and finally gather the results. The automatic setup can perform the same tasks in under 3 minutes, while also freeing up time of the operator and be able to work 24-7.

The robot movement are smooth and few to no errors are encountered during operation. Using functionalities such as force control or external sensors increases reliability, allowing the robot to adapt to from case to case problems and dealing with them effectively. The problem relies in the interpretation of the PLC and the subsequent loss of resolution. The use of a PLC is fundamental to interpret analog signals, establish communication and exchange data with the PC. It's an essential component in any automation system for the versatility of programming and possibilities it offers. In combination with python, organization of data is simple and reliable.

4.1.1 Improvements

Although the cell is functional and operating, resources and time would allow more precision, faster execution and more processing capabilities. Possible improvements in order of importance are discussed here.

The LOGO PLC used is a limiting factor when it comes to measurement precision and number of signals available. Another downside of the LOGO PLC, is the unavailability of two-way communication with the computer. By using a more advanced model such as the S7-300, more functionalities are available, and signals could be manipulated through the Python code directly. The quality of the machine itself is also a factor in determining quality of results. For this reason, modern equipment is required to acquire accurate data. To cut down on cycle time, a possibility is to perform operations with the robot when it is idle. During testing, a new sample can be processed by overlapping two cycles. Although an easy implementation, it could face issues during data logging and the current methodology is not suitable. Occasionally, three-point bending tests must be conducted on small or irregularly shaped components with careful consideration. Currently is not advised to perform test on non-standard samples, as unexpected behaviour can occur. Enhancing the system's adaptability to accommodate a wider variety of sample geometries would significantly broaden its range of potential applications. Adding functionalities is an ongoing process. Introducing diverse test types to be executed in line would allow to gather more data on the single specimen, such as hardness evaluation. Moreover, incorporating automated sample labelling could help reduce manual tasks and improve overall workflow efficiency.

4.2 Tensile test system

The robotic setup was moved near the tensile testing machine and adapted to perform both tensile and bending test. Equipped with a new end effector, the system can execute precise movements by continuously measuring the distance between the gripper and any surrounding surfaces in real time. The testing cycle includes a loading phase into the machine's grippers, initiating and executing the test procedure by communicating with the machine, and removing the fractured parts after test completion.

4.2.1 Improvements

Even if the basic testing cycle is functional, the system is still requires development and needs to be refined before being considered operational.

A proper storage and pick-up station must be implemented to enable continuous operation. This station could also incorporate a dedicated mechanism for spraying the dotted pattern to the sample and ensure correct performance of the surface. Additionally, a measurement station should be integrated to capture not only thickness but also the other sample dimensions.

Another critical aspect is data logging. A lot of data is generated during each test in the form of pictures, and managing this information effectively is still a challenge, particularly in automating the calibration of the DIC camera for each new test. Also, no safety features have been implemented yet, meaning any error would halt the system immediately. For this reason, constant monitoring is advised. Even though the basic operating cycle is functional, this is an ongoing project that still needs refining to be used.

Chapter 5

Conclusion

A fully functional 3-point bending test cell was developed and the ground work for the adaptation to tensile testing laid out. Given the repeatability of the test execution and the precision constantly required, the use of a robotic system is justified. Several challenges still needs to be addressed, but vision of an automatic laboratory is now in the realm of possibility. The hope is that a team of expert, backed up by investments in the field, can finish the work and exponentially increase efficiency.

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Appendix A

Graphs and Images

A.1 Data for Section 2.13

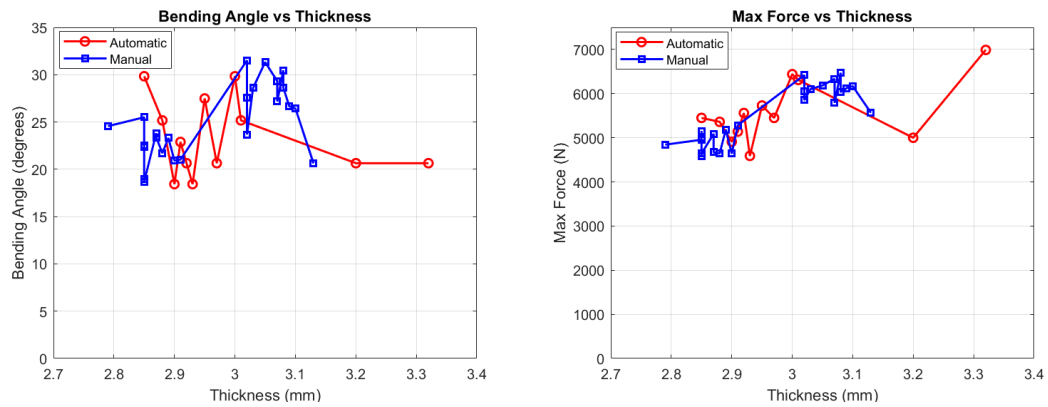


Figure A.1: Bending angle and peak force raw data, plotted with thickness

A.2 Test samples



Figure A.2: Aluminium test sample for bending (left) and tensile(right).

A.3 Robot platform and bending machine

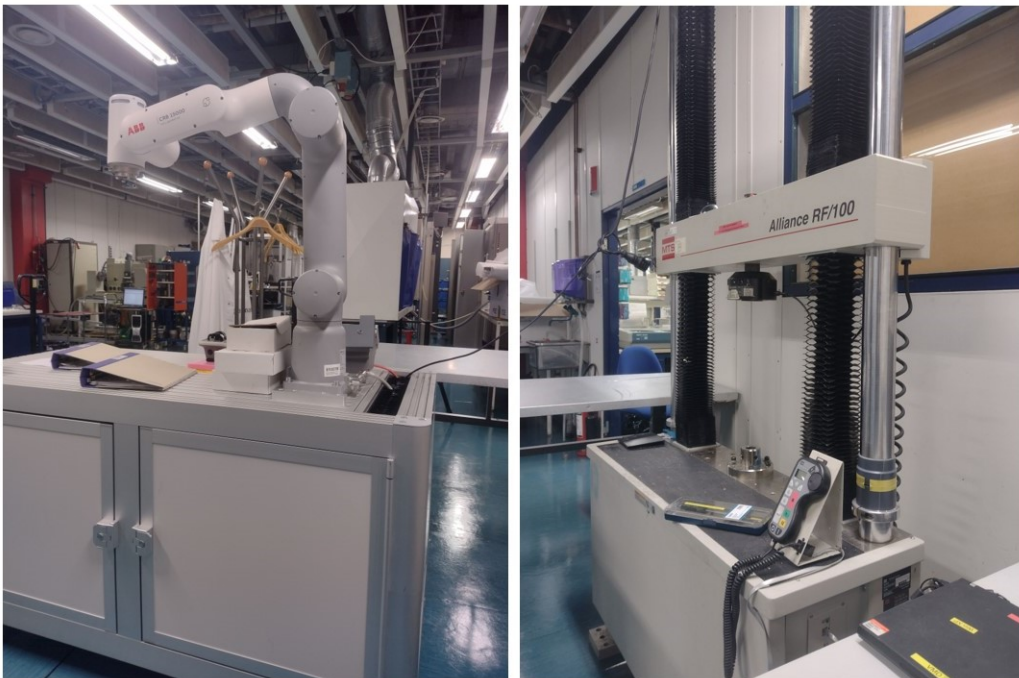


Figure A.3: Robot arm mounted on movable platform (left) and bending machine (right).

Appendix B

Calibration

B.1 Calibration for laser sensor

The calibration line is used to convert the value V , ranging from 0 to 1000 in the PLC memory, to a thickness measurement t_m in mm. Since only a difference in values is representative of a thickness, the line $y = mx + q$ is simplified to $y = mx$. The final relationship used is:

$$t_m = V/3.51 \quad (\text{B.1})$$

(see Appendix C.2, Line 92).

B.2 Calibration of force and crosshead displacement

The calibration for force applied and crosshead displacement is done inside the bending machine software TestWorks 4 and can be customized.

$$F_{max} = 10 \cdot V_F, \quad (\text{B.2})$$

$$S = V_S/3.33 \quad (\text{B.3})$$

F_{max} is the peak force, S the crosshead displacement after preload, and V_F and V_S the corresponding values from 0 to 1000 in the PLC memory (see Appendix C.2, Lines 102 and 123).

Appendix C

Full code

C.1 PLC code

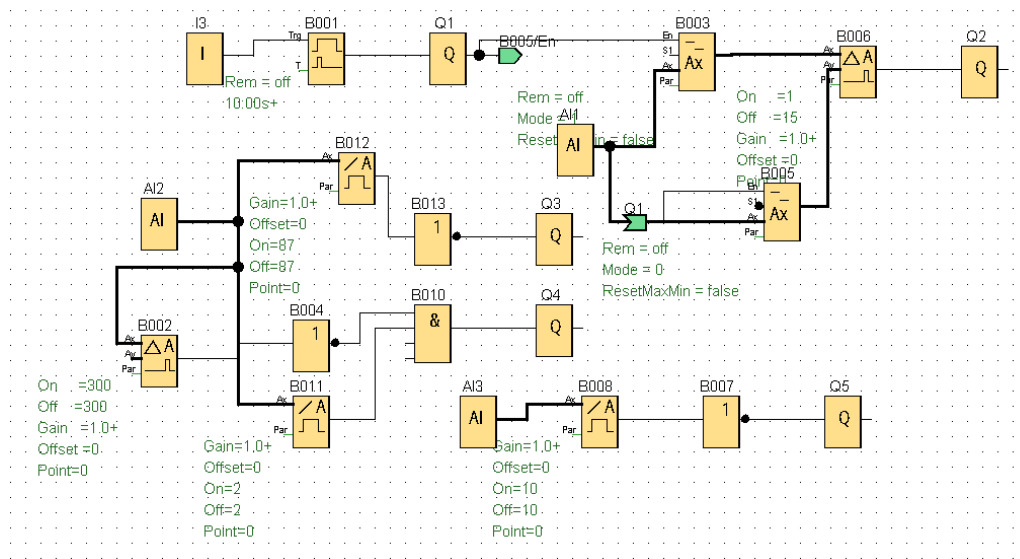


Figure C.1: FBD code for PLC

C.2 Python Code

```
1 import cv2
2 import time
3 import openpyxl
4 import os
5 import pandas as pd
6 import math
7 #import snap7
8 #from snap7.util import set_bool
9 startTime=time.time()
10 count=0
11 # Get the path to the Desktop (works for both Windows and macOS/Linux)
```

```

12 desktop_path = os.path.join(os.path.expanduser("~"), "Desktop", "qr_codes.xlsx")
13 # Check if the Excel file already exists
14 if os.path.exists(desktop_path):
15     # Open the existing Excel file
16     wb = openpyxl.load_workbook(desktop_path)
17     ws = wb.active # Get the active sheet
18 else:
19     # Create a new workbook if the file doesn't exist
20     wb = openpyxl.Workbook()
21     ws = wb.active
22     ws.title = "QR Codes"
23     PLC_IP= '192.168.0.1'
24     DB_Number= 1
25     Byte_index= 0
26     Bit_Index=0
27     #plc= snap7.client.Client()
28     #plc.connect(PLC_IP, 0, 1)
29     bending=True
30     istheFirst=0
31     # Open the camera (0 is usually the default webcam)
32     cap = cv2.VideoCapture(0)
33     # Create a QRCodeDetector object
34     qr_detector = cv2.QRCodeDetector()
35     preloaddisplacement= 591
36     while True:
37         #this part is for adding values in the excel
38         file_path = 'u202aC:\\Users\\S90\\Desktop\\LogFile.csv'
39         cleaned_path = file_path.replace('u202a', '')
40         df = pd.read_csv(cleaned_path)
41         # Capture frame-by-frame
42         ret, frame = cap.read()
43         if not ret:
44             print("Failed to capture image")
45             break
46         # Detect and decode the QR code
47         try:
48             data, bbox, _ = qr_detector.detectAndDecode(frame)
49             # If a QR code is detected and bbox is valid
50             if data and bbox is not None:
51                 # Put the decoded data on the frame
52                 cv2.putText(frame, f'Data: {data}', (50, 50), cv2.FONT_HERSHEY_SIMPLEX, 1, (0, 255, 0), 2)
53                 # Add a 10-second delay after detecting the QR code
54                 print("QR code detected! Creating new line...")
55                 istheFirst=istheFirst+1
56                 #data1=bytearray(plc.db_read(DB_Number, Byte_index, 1))
57                 #set_bool(data1, 0, Bit_Index, True)
58                 #plc.db_write(DB_Number, Byte_index, data1) #changes the value to 1 and activates Q7
59                 time.sleep(10) # Delay for 10 seconds
60                 last_row = df.iloc[-1] # -1 gives the last row
61                 if istheFirst==1:
62                     if last_row['I4']==1: #if the test type is confirmed to be BENDING
63                         ws.append(["New batch - test data - 3 point bending"])
64                         ws.append(["Sample number", "thickness ", "bending angle","max force ","slope"])
65                     elif last_row['I4']==0: #if testtype is confirmed to be tensile
66                         ws.append(["New batch - test data - tensile"])
67                         ws.append(["Sample number", "thickness [mm]","max force [N]"])
68                     #set_bool(data1, 0, Bit_Index, False)
69                     #plc.db_write(DB_Number, Byte_index, data1)
70                     # Append the QR code data to the Excel file
71                     ws.append([data]) # Add the data in a new row of the excel
72                     # Save the workbook to the desktop
73                     wb.save(desktop_path)
74                     print(f"QR code data saved: {data}")
75             except Exception as e:
76                 print(f"Error detecting or decoding QR code: {e}")
77             # Display the frame with QR code data
78             cv2.imshow("QR Code Scanner", frame)
79             last_row = df.iloc[-1] # -1 gives the last row
80             #execute this only if it's a bending test
81             if last_row['I4']==1: #if the test type is confirmed to be BENDING
82                 #Thickness measurement
83                 #this are read from the csv file
84                 last_row = df.iloc[-1] # -1 gives the last row
85                 last_last_row = df.iloc[-2] #gives the row before the last one
86                 last_last_last_row= df.iloc[-3] #third row from the bottom
87                 diff= last_last_row['C4']-last_row['C4'] #this are the correct values for AI1, laser measurement
88                 #print(diff)
89                 if diff>4 and diff<10: #condition to log the difference
90                     #write the diff in the excel
91                     print("log new thickness measurement", diff)
92                     thickness=diff/3.51 #from the calibration, now is in mm
93                     last_row_excel = ws.max_row #gets the last row of the excel file
94                     ws.cell(row=last_row_excel, column=2, value=thickness)

```

```

95         wb.save(desktop_path)
96         time.sleep(5)
97     #logs the max force in excel
98     diff4= last_row['AI3']-last_last_row['AI3']#this are the correct values for AI4, force applied
99     diff5= last_last_row['AI3']- last_last_last_row['AI3']
100     if diff4<0 and diff5>0:
101         print("log new max force", last_last_row['AI3'])
102         maxforce=last_last_row['AI3']*10 #converts the value in N
103         last_row_excel = ws.max_row #gets the last row of the excel file
104         ws.cell(row=last_row_excel , column=4, value=maxforce)
105         wb.save(desktop_path)
106     diff3= last_row['AI3']-last_last_row['AI3']#this are the correct values for AI4, force applied
107     if diff3>0 and last_last_row['AI3']==0:
108         preloaddisplacement=last_last_row['AI2'] #croshead value (in 0-1000)at preload
109         print("new displacement", preloaddisplacement)
110     if (last_row['AI2']-last_last_row['AI2']) !=0:
111         m=((last_row['AI3']-last_last_row['AI3'])*10)/((last_row['AI2']-last_last_row['AI2'])/3.333)
112         if diff3>0 and last_last_row['AI3']<10 and m>0:
113             print("new slope value:", m)
114             last_row_excel = ws.max_row #gets the last row of the excel file
115             ws.cell(row=last_row_excel , column=5, value=m)
116             wb.save(desktop_path)
117     #Bending angle measurement
118     #this are read from the csv file
119     diff2= last_row['AI3']-last_last_row['AI3']#this are the correct values for AI4, force applied
120     if diff2<0 and last_row['AI3']<2: #by making the 2 smaller the measurement is more precise
121         print("log new crosshead position", last_row['AI2'] )
122         disp= last_row['AI2'] -preloaddisplacement #crosshead displacement form preload
123         disp=disp/3.333 #now in mm
124         r=0.4 #mm, punch radius
125         D=30 #mm, roller diameter
126         L=6.09 #mm, roller distance
127         tm=thickness #sample thickness
128         c=(D/2)+tm+r
129         p= (D/2)+(L/2)
130         W= math.sqrt(p**2+(disp-c)**2-c**2)
131         angle= math.degrees(2*math.acos((W*p-c*(disp-c))/(p**2+(disp-c)**2)))
132         last_row_excel = ws.max_row #gets the last row of the excel file
133         ws.cell(row=last_row_excel , column=3, value=angle)
134         wb.save(desktop_path)
135     #execute only if it's a tensile test
136     elif last_row['I4']==0: #if testtype is confirmed to be tensile
137         #this are read from the csv file
138         last_row = df.iloc[-1] # -1 gives the last row
139         last_last_row = df.iloc[-2] #gives the row before the last one
140         last_last_last_row= df.iloc[-3] #third row from the bottom
141         diff5= last_last_row['C4']-last_row['C4']
142         if diff5<0 and last_last_row['C4']==0:
143             startmeasure=time.time()
144         if diff5>0 and last_row['C4']==0:
145             endmeasure=time.time()
146             thickness_=endmeasure-startmeasure #this is the time, needs to be converted to mm
147             print("Logging new thickness value", thickness_)
148             last_row_excel = ws.max_row #gets the last row of the excel file
149             ws.cell(row=last_row_excel , column=3, value=thickness_)
150             wb.save(desktop_path)
151     # Break the loop when 'q' is pressed
152     if cv2.waitKey(1) & 0xFF == ord('q'):
153         break
154     #plc.disconnect()
155     # Release the camera and close all OpenCV windows
156     cap.release()
157     cv2.destroyAllWindows()

```

C.3 Robot code

```

1  MODULE MainModule
2  CONST robtarget pickUp := [[993.12,93.50,136.26],[0.00184305,0.699293,0.714779,-0.00874605],[0,-1,1,0],[9E+09,9E+09,9E
+09,9E+09,9E+09,9E+09]] ;!cups
3  CONST robtarget qrCode := [[949.20,-83.98,47.41],[0.00163261,0.699483,0.714591,-0.00892689],[-1,-1,0,0],[9E+09,9E+09,9E
+09,9E+09,9E+09,9E+09]] ;!cups
4  CONST robtarget before_qrCode := [[782.50,-83.94,47.35],[0.00158366,0.699486,0.714589,-0.0089546],[ -1,-1,0,0],[9E+09,9
E+09,9E+09,9E+09,9E+09,9E+09]] ;!cups
5  CONST robtarget before_pickUp := [[969.36,93.38,162.60],[0.00181894,0.699326,0.714746,-0.00878559],[0,-1,1,0],[9E+09,9
E+09,9E+09,9E+09,9E+09,9E+09]] ;!cups
6  CONST robtarget after_pickUp := [[841.00,93.28,162.49],[0.00175594,0.699364,0.714709,-0.00884688],[0,-1,1,0],[9E+09,9E
+09,9E+09,9E+09,9E+09,9E+09]] ;!cups
7  VAR robtarget currentPos;
8  CONST robtarget before_measurement:=
[[729.36,-267.85,298.45],[0.00161964,0.699505,0.714571,-0.00890977],[-1,-1,0,0],[9E+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ;!cups

```

```

E+09]] ; !cups
9  CONST robtarget measurement:= [[748.22,-368.08,203.29],[0.113901,-0.670866,-0.668719,0.299633],[-1,-1,0,0],[9E+09,9E
+09,9E+09,9E+09,9E+09,9E+09]] ; !cups
10 CONST robtarget after_measurement := [[807.31,-314.79,110.04],[0.128322,-0.689958,-0.626499,0.339101],[-1,-1,0,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ; !cups
11 CONST robtarget after_testing:= [[-814.21,-103.97,81.26],[0.00509138,-0.711578,-0.701649,-0.0363391],[-2,-1,-1,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ; !gripper
12 CONST robtarget disposal_pickUp :=
[[-1052.97,-113.96,17.09],[0.00502324,-0.706542,-0.70764,-0.00431698],[-2,-1,-1,0],[9E+09,9E+09,9E+09,9E+09,9E
+09,9E+09]] ; !gripper
13 CONST robtarget disposal:= [[-86.18,-499.14,18.58],[0.0190478,-0.715392,0.698397,0.00969954],[-2,-1,1,0],[9E+09,9E
+09,9E+09,9E+09,9E+09,9E+09]] ; !gripper
14 PERS tooldata cups := [TRUE,[[0,250,70.5],[1,0,0,0]],[0.3,[0,0,45],[1,0,0,0],0.000076,0.00569,0.00577]] ;
15 PERS tooldata gripper := [TRUE,[[0,-242,115.8],[1,0,0,0]],[0.3,[0,0,45],[1,0,0,0],0.000076,0.00569,0.00577]] ;
16 CONST robtarget before_testing := [[-824.05,-107.80,126.28],[0.0363917,-0.703476,0.709768,0.00503275],[-2,-1,1,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ; !cups
17 CONST robtarget testing := [[-1026.92,-111.82,8.26],[0.00132636,0.779113,-0.626878,0.00233852],[-2,0,0,0],[9E+09,9E+09,9E
+09,9E+09,9E+09,9E+09]] ; !cups
18 CONST robtarget midwaytesting1 := [[633.51,-617.37,426.98],[0.00765945,0.850706,0.519315,-0.0809479],[-1,-1,0,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ; !cups
19 CONST robtarget midwaytesting2 := [[-487.59,-738.07,426.94],[0.0457086,-0.986518,0.142026,0.067248],[-2,-1,0,0],[9E+09,9E
+09,9E+09,9E+09,9E+09,9E+09]] ; !cups
20 CONST robtarget return1 := [[-329.57,-509.56,545.56],[0.0190071,-0.715366,0.698424,0.00970655],[-2,-1,1,0],[9E+09,9E
+09,9E+09,9E+09,9E+09,9E+09]] ; !tool0
21 CONST robtarget return2 := [[300.53,-527.21,545.53],[0.0112175,-0.974053,0.225311,0.0181802],[-1,-1,1,0],[9E+09,9E+09,9E
+09,9E+09,9E+09,9E+09]] ; !tool0
22 CONST robtarget return3 := [[365.46,-394.59,545.53],[0.021308,-0.739627,-0.672679,0.00112997],[-1,-1,0,0],[9E+09,9E+09,9E
+09,9E+09,9E+09,9E+09]] ; !tool0
23 CONST robtarget return4 := [[446.03,79.01,587.76],[0.0213177,-0.739603,-0.672705,0.00115511],[0,0,1,0],[9E+09,9E+09,9E
+09,9E+09,9E+09,9E+09]] ; !tool0
24 PERS loaddata my_load:= [0.001,[0,0,0.001],[1,0,0,0],0,0,0] ;
25 CONST robtarget after_qrCode := [[729.24,-91.73,228.01],[0.0017099,0.699398,0.714675,-0.00887841],[-1,-1,0,0],[9E+09,9E
+09,9E+09,9E+09,9E+09,9E+09]] ;
26 VAR num completedcycleCount_bending := 0 ;
27 VAR num completedcycleCount_tensile := 0 ;
28 VAR num n_first_stack:=12 ; !change to 0 if the user inputs it
29 CONST robtarget pickUp2 := [[987.17,183.74,127.66],[0.00180553,0.699512,0.714563,-0.00891453],[0,-1,1,0],[9E+09,9E
+09,9E+09,9E+09,9E+09,9E+09]] ;
30 VAR robtarget disposal_error ;
31 CONST robtarget beforedisposal1 := [[-610.29,-125.48,154.84],[0.0221359,-0.975715,-0.216719,-0.0228719],[-2,-1,0,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ;
32 VAR num testtype:=0 ;
33 CONST robtarget beforedisposal2 := [[-86.29,-474.07,149.95],[0.0189831,-0.715332,0.69846,0.0096874],[-2,-1,1,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ;
34 VAR robtarget pOffsetTarget ;
35 CONST robtarget tens_before_pickUp := [[861.46,26.96,126.66],[0.00420267,0.0314857,0.99943,-0.011459],[0,-1,0,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ;
36 CONST robtarget tens_pickUp := [[870.14,88.35,42.13],[0.00960392,-0.0165421,0.999541,-0.0235006],[0,-1,0,0],[9E+09,9E
+09,9E+09,9E+09,9E+09,9E+09]] ;
37 CONST robtarget tens_after_pickUp := [[390.28,129.12,400.92],[0.444508,-0.52413,-0.510271,0.517033],[0,0,1,0],[9E+09,9E
+09,9E+09,9E+09,9E+09,9E+09]] ;
38 PERS tooldata softGripper := [TRUE,[[0,0,300],[1,0,0,0]],[0.1,[0,0,45],[1,0,0,0],0.000076,0.00569,0.00577]] ;
39 CONST robtarget tens_before_qrCode := [[842.16,-76.65,79.42],[0.0109854,0.717299,0.696658,-0.00529772],[-1,-1,0,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ;
40 CONST robtarget tens_after_qrCode := [[662.54,-75.24,104.81],[0.421883,-0.512219,0.569136,-0.485521],[-1,-2,0,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ;
41 CONST robtarget tens_qrCode := [[897.79,-76.68,47.80],[0.0109815,0.717302,0.696656,-0.00530085],[-1,-1,0,0],[9E+09,9E
+09,9E+09,9E+09,9E+09,9E+09]] ;
42 CONST robtarget tensbeforemeasurement := [[902.84,-171.58,166.97],[0.32982,0.169322,0.477976,-0.796296],[0,-2,0,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ;
43 CONST robtarget tensaftermeasurement := [[873.84,-171.67,166.91],[0.329766,0.169317,0.477997,-0.796307],[0,-2,1,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ;
44 CONST robtarget tenshome := [[505.76,-76.38,572.84],[0.0241064,0.72101,0.690225,-0.0561474],[-1,-1,0,0],[9E+09,9E+09,9E
+09,9E+09,9E+09,9E+09]] ;
45 CONST robtarget tens_midwaytesting1 := [[61.28,-693.78,528.06],[0.0958796,-0.0601222,0.720197,-0.684477],[-1,1,1,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ;
46 CONST robtarget tens_midwaytesting2 := [[-636.49,-282.80,528.07],[0.319913,-0.369766,-0.620939,0.612669],[-2,1,1,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ;
47 CONST robtarget tens_testing := [[-1089.38,-189.56,96.20],[0.330586,-0.37914,-0.600713,0.621378],[-2,1,1,0],[9E+09,9E
+09,9E+09,9E+09,9E+09,9E+09]] ;
48 CONST robtarget tens_beforeTesting := [[-1017.51,-315.88,96.18],[0.330597,-0.379166,-0.600709,0.62136],[-2,1,1,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ;
49 CONST robtarget tens_duringTesting := [[-943.35,-118.66,96.13],[0.389514,-0.447151,-0.560054,0.57851],[-2,1,1,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ;
50 CONST robtarget tens_disposal_upper :=
[[-1067.91,-183.78,139.27],[0.368677,-0.354257,-0.621869,0.593176],[-2,1,1,0],[9E+09,9E+09,9E+09,9E+09,9E+09,9E
+09]] ;
51 CONST robtarget tens_disposal_lower := [[-1061.65,-173.36,86.28],[0.33724,-0.411471,-0.598387,0.599077],[-2,1,1,0],[9E
+09,9E+09,9E+09,9E+09,9E+09,9E+09]] ;
52 CONST robtarget tens_disposal_general :=
[[-269.14,-129.66,52.68],[0.0175953,0.0412698,0.998137,-0.0413612],[-2,0,2,0],[9E+09,9E+09,9E+09,9E+09,9E+09,9E
+09]] ;
53 CONST robtarget tens_disposal_upper_afterpickup :=

```



```

[[ -719.33, 142.16, 80.80 ], [ 0.364359, -0.365372, -0.621605, 0.589366 ], [ 1, 1, 1, 0 ], [ 9E+09, 9E+09, 9E+09, 9E+09, 9E
+09 ]];
54 CONST robtarget tens_disposal_lower_afterpickup :=
[[ -719.33, 142.16, 80.80 ], [ 0.364359, -0.365372, -0.621605, 0.589366 ], [ 1, 1, 1, 0 ], [ 9E+09, 9E+09, 9E+09, 9E+09, 9E
+09 ]];
55 !CONST robtarget tens_midwaydisposal :=
[[ -417.31, -178.46, 356.09 ], [ 0.0685055, -0.211178, 0.755584, -0.616283 ], [ 1, 0, 1, 0 ], [ 9E+09, 9E+09, 9E+09, 9E+09, 9E
+09 ]];
56 CONST robtarget tens_midwaydisposal := [[ -718.61, -247.19, 322.68 ], [ 0.337264, -0.411542, -0.598363, 0.599039 ], [ -2, 1, 1, 0 ], [ 9
E+09, 9E+09, 9E+09, 9E+09, 9E+09 ]];
57 CONST robtarget tens_midwaydisposal2 := [[ -805.92, -208.46, 159.85 ], [ 0.341957, -0.36695, -0.643607, 0.578086 ], [ -2, 1, 1, 0 ], [ 9
E+09, 9E+09, 9E+09, 9E+09, 9E+09 ]];
58 PROC main()
59   reset_all_scalableD0;
60   RESET ABB_Scalable_IO_0_D016; !has to reset testType from the previous cycle
61   IF completedcycleCount_bending=0 AND completedcycleCout_tensile=0 THEN
62     TPErase;
63     TPReadFK testtype, "What type of test will be executed? ", "Bending", "Tensile", "trial", stEmpty, stEmpty;
64   ENDIF
65   IF testtype = 1 THEN
66     SET ABB_Scalable_IO_0_D016; !this is the verification for bending test
67     pickUp_procedure_bending;
68     qrCode_procedure_bending;
69     measurement_procedure_bending;
70     testing_procedure_bending;
71     disposal_procedure_bending;
72     return_procedure_bending;
73   ELSEIF testtype = 2 THEN
74     pickUp_procedure_tensile;
75     qrCode_procedure_tensile;
76     measurement_procedure_tensile;
77     testing_procedure_tensile;
78     disposal_procedure_tensile;
79   ELSEIF testtype= 3 THEN
80     MoveJ tens_before_pickUp, v50, z0, softGripper; !goes to home position
81     WaitTime 1;
82     currentPos := CRobT(); ! Get current position
83     WHILE ABB_Scalable_IO_0_DI6 = 0 DO !until laser detect correct position on the z
84       MoveL Offs(currentPos, -5, -5, 0), v50, z0, softGripper; ! Move in steps of 5 mm
85       currentPos := CRobT(); ! Update current position
86     ENDWHILE
87     WaitTime 1;
88   ELSE
89     ErrRaise "Custom error", 90001, "error", "error", "error", "error", "error";
90   ENDIF
91   ERROR !deals with errors in the entire code
92   TPWrite "An error occurred, trying reset...";
93   IF ABB_Scalable_IO_0_DI1 =1 THEN !detects if the vacuum is on(there's a sample attached)
94     MoveJ disposal_error, v50, z0, cups;
95     RESET ABB_Scalable_IO_0_D02; !deactivates vacuum
96     SET ABB_Scalable_IO_0_D03; !activates and deactivates blow off
97     WaitTime 1;
98     RESET ABB_Scalable_IO_0_D03;
99   ENDIF
100   MoveJ wi_homePosition, v50, z0, tool0; !goes to home position
101   StartMoveRetry; !restats the program
102 ENDPROC
103 PROC pickUp_procedure_bending()
104   MoveL before_pickUp, v50, z0, cups;
105   IF completedcycleCount_bending=0 THEN
106     !TPReadNum n_first_stack, "How many samples are there in the first stack?";
107   ENDIF
108   IF completedcycleCount_bending < n_first_stack THEN !picks up only the correct number of samples from the first
stack
109     MoveL pickUp, v20, z0, cups;
110   ELSE
111     MoveL pickUp2, v20, z0, cups;
112   ENDIF
113   SET ABB_Scalable_IO_0_D02; !activates vacuum
114   currentPos := CRobT(); ! Get current position
115   WHILE ABB_Scalable_IO_0_DI1 = 0 DO !until vacuum is detected, goes down
116     MoveL Offs(currentPos, 0, 0, -10), v20, z0, cups; ! Move down in steps of 10 mm
117     currentPos := CRobT(); ! Update current position
118   ENDWHILE
119   IF completedcycleCount_bending < n_first_stack THEN
120     MoveL pickUp, v20, z0, cups; !goes back up straight, to not move the samples below
121   ELSE
122     MoveL pickUp2, v20, z0, cups;
123   ENDIF
124   MoveL after_pickUp, v100, z0, cups;
125 ENDPROC
126 PROC qrCode_procedure_bending()
127   MoveL before_qrCode, v200, z0, cups;

```

```

128     MoveL qrCode, v200, z0, cups;
129     WaitTime 7; !reads QR-code
130     MoveL before_qrCode, v200, z0, cups;
131     MoveL after_qrCode, v200, z0, cups;
132 ENDPROC
133 PROC measurement_procedure_bending()
134     MoveL before_measurement, v200, z0, cups;
135     MoveL measurement, v100, z0, cups;
136     SET ABB_Scalable_IO_0_D05; ! this is the output doMeasurement seen in the PLC as doMeasure, I1
137     WaitTime 5;
138     RESET ABB_Scalable_IO_0_D02; !deactivates vacuum
139     SET ABB_Scalable_IO_0_D03; !activates and deactivates blow off
140     WaitTime 1;
141     RESET ABB_Scalable_IO_0_D03;
142     WaitTime 5; !waits for the measurement to take place until the end
143     !WaitDI ABB_Scalable_IO_0_DI3, 1, \MaxTime:=30; !waits the input continueTest_measurement from the PLC, maxtime 1 min,
       after calls the error handler !deactivated
144     MoveL after_measurement, v50, z0, cups; ! goes to pick up the sample after measurement
145     FCRefForce \Fz:=-5; ! Setup the force reference with 5N in Z-direction of the world frame
146     FCAct cups; ! Activate Force Control
147     FCRefStart; ! Start moving the robot to achieve the specified force
148     WaitTime 10;
149     SET ABB_Scalable_IO_0_D02; !activates vacuum
150     FCRefStop; ! Stop the reference values
151     FCDeact; ! Deactivate force control
152     MoveL before_measurement, v100, z0, cups;
153     RESET ABB_Scalable_IO_0_D05; !resets output doMeasurement to be ready for next cycle
154     RESET ABB_Scalable_IO_0_D05; !deactivates the plc circuit to do the measurement
155 ENDPROC
156 PROC testing_procedure_bending()
157     MoveJ midwaytesting1, v1000, z0, cups;
158     MoveJ midwaytesting2, v1000, z0, cups;
159     MoveJ before_testing, v1000, z0, cups; !moves into the testing area
160     MoveL testing, v50, z0, cups;
161     WaitTime 3;
162     RESET ABB_Scalable_IO_0_D02; !deactivates vacuum
163     SET ABB_Scalable_IO_0_D03; !activates and deactivates blow off
164     WaitTime 1;
165     RESET ABB_Scalable_IO_0_D03;
166     MoveL testing, v50, z0, cups;
167     MoveL before_testing, v50, z0, cups; !gets out of the way
168     WaitDI ABB_Scalable_IO_0_DI4, 1, \MaxTime:=120; !positon check
169     TPWrite "Position check passed, test starts in 5 seconds";
170     WaitTime 5;
171     SET ABB_Scalable_IO_0_D012; !this is start test
172     MoveJ after_testing, v100, z0, gripper; !turns the tool around
173     RESET ABB_Scalable_IO_0_D012; !this needed to be reset
174 ENDPROC
175 PROC disposal_procedure_bending()
176     WaitDI ABB_Scalable_IO_0_DI7, 1, \MaxTime:=300; !waits for the test to be finished
177     MoveL disposal_pickUp, v100, z0, gripper;
178     WaitTime 2;
179     SET ABB_Scalable_IO_0_D06; !closes the gripper
180     MoveL after_testing, v100, z0, gripper;
181     MoveL beforedisposal1, v100, z0, gripper;
182     MoveL beforedisposal2, v100, z0, gripper;
183     IF completedcycleCount_bending<6 THEN
184         pOffsetTarget := disposal; ! Copy original position
185         pOffsetTarget.trans := disposal.trans + [80*completedcycleCount_bending, 0, 0]; ! Add 60mm in X per completed cycle
186         MoveL pOffsetTarget, v50, z0, gripper;
187         RESET ABB_Scalable_IO_0_D06; !drops tested sample
188     ELSEIF completedcycleCount_bending>5 AND completedcycleCount_bending<12 THEN
189         pOffsetTarget := disposal; ! Copy original position
190         pOffsetTarget.trans := disposal.trans + [80*(completedcycleCount_bending-6), 40, 0]; ! Add 60mm in X per completed
           cycle
191         MoveL pOffsetTarget, v50, z0, gripper;
192         RESET ABB_Scalable_IO_0_D06; !drops tested sample
193     ELSE
194         pOffsetTarget := disposal; ! Copy original position
195         pOffsetTarget.trans := disposal.trans + [80*(completedcycleCount_bending-12), 80, 0]; ! Add 60mm in X per completed
           cycle
196         MoveL pOffsetTarget, v50, z0, gripper;
197         RESET ABB_Scalable_IO_0_D06; !drops tested sample
198     ENDIF
199 ENDPROC
200 PROC return_procedure_bending()
201     MoveL return1, v300, z0, tool0;
202     MoveJ return2, v300, z0, tool0;
203     MoveJ return3, v300, z0, tool0;
204     MoveJ return4, v300, z0, tool0;
205     completedcycleCount_bending := completedcycleCount_bending + 1; !counts the number of cycles
206 ENDPROC
207 PROC reset_all_scalableD0()

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208 RESET ABB_Scalable_IO_0_D01;
209 RESET ABB_Scalable_IO_0_D02;
210 RESET ABB_Scalable_IO_0_D03;
211 RESET ABB_Scalable_IO_0_D04;
212 RESET ABB_Scalable_IO_0_D05;
213 RESET ABB_Scalable_IO_0_D06;
214 RESET ABB_Scalable_IO_0_D07;
215 RESET ABB_Scalable_IO_0_D08;
216 RESET ABB_Scalable_IO_0_D09;
217 RESET ABB_Scalable_IO_0_D010;
218 RESET ABB_Scalable_IO_0_D011;
219 RESET ABB_Scalable_IO_0_D012;
220 RESET ABB_Scalable_IO_0_D013;
221 RESET ABB_Scalable_IO_0_D014;
222 RESET ABB_Scalable_IO_0_D015;
223 RESET ABB_Scalable_IO_0_D016;
224 ENDPROC
225 PROC pickUp_procedure_tensile()
226 MoveL tens_before_pickUp, v100, z0, softGripper;
227 WaitTime 1;
228 currentPos := CRobT(); ! Get current position
229 WHILE ABB_Scalable_IO_0_DI6 = 0 DO !until laser detect correct position, goes down
230 MoveL Offs(currentPos, 0, 0, -5), v10, z0, softGripper; ! Move down in steps of 5 mm
231 currentPos := CRobT(); ! Update current position
232 ENDWHILE
233 WaitTime 1;
234 SET ABB_Scalable_IO_0_D015; !closes the soft gripper
235 MoveL tens_before_pickUp, v100, z0, softGripper;
236 ENDPROC
237 PROC qrCode_procedure_tensile()
238 MoveJ tens_before_qrCode, v100, z0, softGripper;
239 MoveL tens_qrCode, v100, z0, softGripper;
240 WaitTime 7; !wait for QR-code detection
241 MoveL tens_before_qrCode, v100, z0, softGripper;
242 ENDPROC
243 PROC measurement_procedure_tensile()
244 MoveJ tensbeforemeasurement, v20, z0, softGripper;
245 MoveL tensaftermeasurement, v5, z0, softGripper; !does the measurement, recod the time
246 MoveJ tenshome, v100, z0, softGripper;
247 ENDPROC
248 PROC testing_procedure_tensile()
249 MoveJ tens_midwaytesting1, v300, z0, softGripper;
250 MoveJ tens_midwaytesting2, v300, z0, softGripper;
251 MoveJ tens_beforeTesting, v300, z0, softGripper; !right above the machine lower gripper
252 MoveL tens_testing, v30, z0, softGripper;
253 SET ABB_Scalable_IO_0_D09; !this is close the lower gripper on the machine
254 WaitTime 3; !closes for 3 seconds
255 RESET ABB_Scalable_IO_0_D09; !the gripper finished the closing procedure
256 WaitTime 2;
257 RESET ABB_Scalable_IO_0_D015; !opens the soft gripper
258 MoveL tens_duringTesting, v50, z0, softGripper;
259 WaitTime 1;
260 SET ABB_Scalable_IO_0_D010; !this is start test on the machine (with the finger)
261 WaitTime 3;
262 RESET ABB_Scalable_IO_0_D010;
263 WaitTime 15; !waits
264 SET ABB_Scalable_IO_0_D013; !close the upper gripper
265 WaitTime 3;
266 RESET ABB_Scalable_IO_0_D013;
267 TPWrite "Test starting...";
268 !execute test
269 ENDPROC
270 PROC disposal_procedure_tensile()
271 WaitDI ABB_Scalable_IO_0_DI9, 1; !test finished and grippers in position
272 MoveL tens_disposal_lower, v50, z0, softGripper;
273 WaitTime 1;
274 currentPos := CRobT(); ! Update current position
275 WHILE ABB_Scalable_IO_0_DI6 = 0 DO !until laser detect correct position
276 MoveL Offs(currentPos, -10, -5, 0), v10, z0, softGripper; ! Move in steps of 5 mm
277 currentPos := CRobT(); ! Update current position
278 ENDWHILE
279 WaitTime 1;
280 SET ABB_Scalable_IO_0_D015; !closes the soft gripper
281 WaitTime 1;
282 SET ABB_Scalable_IO_0_D011; !opens the lower gripper
283 WaitTime 3;
284 RESET ABB_Scalable_IO_0_D011;
285 MoveL tens_beforeTesting, v20, z0, softGripper; !this point is on the side
286 MoveJ tens_midwaydisposal, v100, z0, softGripper;
287 MoveJ tens_disposal_general, v100, z0, softGripper;
288 WaitTime 1;
289 RESET ABB_Scalable_IO_0_D015; !opens the soft gripper
290 WaitTime 1;

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291 MoveL tens_midwaydisposal, v100, z0, softGripper;
292 MoveJ tens_midwaydisposal2, v100, z0, softGripper;
293 MoveL tens_disposal_upper, v50, z0, softGripper;
294 WaitTime 1;
295 currentPos := CRobT(); ! Get current position
296 WHILE ABB_Scalable_IO_0_DI6 = 0 DO !until laser detect correct position
297     MoveL Offs(currentPos, -10, -5, 0), v10, z0, softGripper; ! Move in steps of 5 mm
298     currentPos := CRobT(); ! Update current position
299 ENDWHILE
300 WaitTime 1;
301 SET ABB_Scalable_IO_0_D015; !closes the soft gripper
302 WaitTime 1;
303 SET ABB_Scalable_IO_0_D014; !opens the upper gripper
304 WaitTime 3;
305 RESET ABB_Scalable_IO_0_D014; !finish opeining the upper gripper
306 MoveL tens_beforeTesting, v20, z0, softGripper; !this point is on the side
307 MoveL tens_midwaydisposal, v100, z0, softGripper;
308 MoveJ tens_disposal_general, v100, z0, softGripper;
309 WaitTime 1;
310 RESET ABB_Scalable_IO_0_D015; !opens the soft gripper, drop sample
311 WaitTime 1;
312 MoveJ tens_midwaytesting2, v300, z0, softGripper;
313 MoveJ tens_midwaytesting1, v300, z0, softGripper;
314 MoveJ tenshome, v300, z0, tool0;
315 completedcycleCout_tensile:=completedcycleCout_tensile+1; !counts the number of cycles of tensile
316 ENDPROC
317 ENDMODULE

```